### 4.1.3 FOCAL LENGTH AND DISTORTION

### 4.1.3.1 NAC FM FOCAL LENGTH AND DISTORTION MEASUREMENTS

As reported in Reference 4.1.3.1-1

## Reference 4.1.3.1-1 - IOM , 'NAC Flight Model Focal Length And Distortion Measurement Results'", Edward Motts, August 26, 1998

### 4.1.3.1.1 SCOPE

This report describes a measurement of the Cassini Narrow Angle Camera Flight Model (NAC F/M) performed on November 9, 1995. The objective of the measurement was to determine Effective Focal Length (EFL) and field distortion of the camera optics. Measurement results were apparently not distributed at the time of the test; this memorandum is therefore intended as the final test report.

The accuracy requirement for the focal length is defined in Cassini document 699-CAS-5-2036-CAL, Imaging Science Subsystem (ISS) Instrument Calibration Requirements Document, Component Level Calibrations as $\pm 0.5 \mathrm{~mm}$. No requirement is established for field distortion at the component level.

The measured EFL is $2000 \mathrm{~mm}, \pm 4 \mathrm{~mm}(3 \sigma)$. Field distortion is less than can be measured by this technique.

### 4.1.3.1.2 DESCRIPTION OF TEST METHOD

Measurements of the angles between the NAC/WAC tooling plate optical cube and the NAC grid target were performed using electronic optical theodolites. The theodolites measured angles in a horizontal plane in reference to a porroprism. Angles in a vertical plane were measured with respect to local gravity. Theodolite angles were recorded using a portable computer running the Leica ManCAT software. Refer to Figure 4.1.3.1-1 for the instrument layout.

Determinations of the tooling plate optical cube $-X$ and $+Z$ face normals were performed by autocollimation to those faces. Determination of each grid target location was performed by superimposing the theodolite telescope reticle over the grid intersection. Each data point recorded was the mean of ten individual observations. Refer to Figure 4.1.3.1-2 for grid intersection locations.

Database file "NACFL2.dbf" containing all measured angles was exported to Excel spreadsheet "ISSDIST.xIs" sheet 4 for data reduction.

### 4.1.3.1.3 DATA REDUCTION

Database files were imported into the Excel spreadsheet "ISSDIST.xls" as described above. Refer to Table 4.1.3.1-1 for raw data.

Angle $\varphi$ (the angle in the plane containing a given grid intersection and the center grid intersection) was calculated as the RSS of the two component angles:

$$
\varphi=\sqrt{\left(\Delta H z^{2}+\Delta V^{2}\right)}
$$

Table 4.1.3.1-2 contains calculated values of angle $\varphi$ for each grid intersection. Radial distances " $h$ '" to each grid intersection were calculated from drawing dimensions and are also contained in Table 4.1.3.1-2.

$$
E F L=\frac{h^{\prime}}{\tan \varphi}
$$

The effective focal length (EFL) was calculated using h' and $\varphi$ for each grid intersection: Finally, the percentage distortion to a corner target intersection (such as point B1) is calculated as the percent deviation from the paraxial focal length:

$$
\% \text { distortion }=\frac{E F L_{B I}-E F L_{\text {parax. }} .}{E F L_{\text {parax. }}} * 100 \%
$$

### 4.1.3.1.4 UNCERTAINTY ESTIMATE

Random error was estimated by calculating the standard deviation of the theodolite observations. The value of angle _ was then perturbed by the standard deviation to determine the effect on EFL. Then, the EFL equation was perturbed by the stated uncertainty of the grid target, $\pm 0.25 \mu \mathrm{~m}$. The two random error contributions were then combined by the Root Sum Square (RSS) method. Finally, the RSS was multiplied times three to give a $\pm$ three $\sigma$ uncertainty estimate.

The measurement uncertainty in EFL is inversely proportion to the radial distance h.
Please note that the uncertainty value reported is for the greatest value of $h$, at the ends of the diagonal lines.

The calculated measurement uncertainty in the measured focal length is $\pm 4.4 \mathrm{~mm}(3 \sigma)$. Estimation of the uncertainty (error) in the reported angles was accomplished in spreadsheet "ISSDIST.xIs" sheet 4 and is shown in Table 4.1.3.1-3 of this report.

### 4.1.3.1.5 TEST RESULTS

The calculated focal lengths are shown in Table 4.1.3.1-2. Figure 4.1.3.1-3 graphically represents the measured values. The best fit line of Figure 3 crosses the vertical axis at $2000 \pm 4 \mathrm{~mm}$ (three $\sigma$ ), the expected paraxial focal length. The EFL at point B1 is 2000.8. The calculated field distortion is $0.04 \%$. In other words, the field distortion is less than can be measured by this method.

Note that the estimated measurement uncertainty of $\pm 4.4 \mathrm{~mm}$ (three $\sigma$ ) does not meet the Component Level Calibrations requirement of $\pm 0.5 \mathrm{~mm}$ accuracy.


Figure 4.1.3.1-1 - Instrument Layout



IDENTIFICATION OF GRID INTERSECTION POINTS

Figure 4.1.3.1-2 - Grid Target Intersection Points and Identification

| A1 | 90.75290 | 90.05154 |
| :---: | :---: | :---: |
| A2 | 90.79586 | 90.05150 |
| A3 | 90.83893 | 90.05153 |
| A4 | 90.88187 | 90.05150 |
| A5 | 90.93211 | 90.04437 |
| A6 | 90.98250 | 90.03696 |
| A7 | 91.02545 | 90.03692 |
| A8 | 91.06850 | 90.03695 |
| A9 | 91.11143 | 90.03692 |
| B1 | 90.75363 | 89.86427 |
| B2 | 90.79647 | 89.90720 |
| B3 | 90.83932 | 89.95028 |
| B4 | 90.88227 | 89.99336 |
| B5 | 90393235 | 90.04351 |
| B6 | 90.98243 | 90.09365 |
| B7 | 91.02538 | 90.13667 |
| B8 | 91.06820 | 90.17963 |
| B9 | 91.11107 | 90.22251 |
| C1 | 90.95269 | 89.86401 |
| C2 | 90.92547 | 89.90695 |
| C3 | 90.92544 | 89.94999 |
| C4 | 90.92553 | 89.99294 |
| C5 | 90.93256 | 90.04309 |
| C6 | 90.93958 | 90.09305 |
| C7 | 90.93949 | 90.13598 |
| C8 | 90.93938 | 90.17898 |
| C9 | 90.93927 | 90.22192 |
| D1 | 91.11178 | 89.86408 |
| D2 | 91.06878 | 89.90689 |
| D3 | 91.05271 | 89.94896 |
| D4 | 90.98271 | 89.99281 |
| D5 | 90.93253 | 90.04284 |
| D6 | 90.88226 | 90.09275 |
| D7 | 90.83919 | 90.13568 |
| D8 | 90.79620 | 90.17853 |
| D9 | 90.75310 | 90.22127 |
| PORROB1 | 1.00008 | 106.73701 |
| PORROC1 | 0.99569 | 91.19378 |
| CUBEX1 | 191.5627 | 89.98797 |
| CUBEZ1 | 90.99742 | 90.00739 |

Table 4.1.3.1-1 - Raw Data : NAC Flight Model Focal Length and Distortion Measurements

| GRID INTERSECTION POINT | $\begin{gathered} \hline \text { phi } \\ \text { (radians) } \end{gathered}$ | $h^{\prime \prime}$ (mm) | EFL (mm) |
| :---: | :---: | :---: | :---: |
| A1 | 0.00313 | 6.254988 | 1998.2 |
| A2 | 0.002381 | 4.75674 | 1997.5 |
| A3 | 0.001631 | 3.259601 | 1998.5 |
| A4 | 0.000886 | 1.767767 | 1996.0 |
| A5 |  |  |  |
| A6 | 0.000889 | 1.767767 | 1988.6 |
| A7 | 0.001634 | 3.259601 | 1994.6 |
| A8 | 0.002384 | 4.756574 | 1995.3 |
| A9 | 0.003132 | 6.254998 | 1996.9 |
| B1 | 0.004418 | 8.838834 | 2000.8 |
| B2 | 0.003359 | 6.717514 | 1999.8 |
| B3 | 0.002299 | 4.596194 | 1999.5 |
| B4 | 0.001237 | 2.474873 | 2000.7 |
| B5 |  |  |  |
| B6 | 0.001237 | 2.474873 | 2000.8 |
| B7 | 0.002298 | 4.596194 | 2000.1 |
| B8 | 0.0.003356 | 6.717514 | 2001.3 |
| B9 | 0.004415 | 8.838834 | 2002.1 |
| C1 | 0.003128 | 6.254998 | 1999.8 |
| C2 | 0.002379 | 4.756574 | 1999.1 |
| C3 | 0.00163 | 3.259601 | 2000.0 |
| C4 | 0.000884 | 1.767767 | 1999.7 |
| C5 |  |  |  |
| C6 | 0.00088 | 1.767767 | 2007.8 |
| C7 | 0.001626 | 3.259601 | 2005.2 |
| C8 | 0.002375 | 4.756574 | 2003.1 |
| C9 | 0.003123 | 6.254998 | 2002.7 |
| D1 | 0.004418 | 8.838834 | 2000.5 |
| D2 | 0.003359 | 6.717514 | 1999.7 |
| D3 | 0.002298 | 4.596194 | 2000.5 |
| D4 | 0.001237 | 2.474873 | 2001.2 |
| D5 |  |  |  |
| D6 | 0.001236 | 2.474873 | 2001.9 |
| D7 | 0.002298 | 4.596194 | 2000.4 |
| D8 | 0.003357 | 6.717514 | 2001.0 |
| D9 | 0.004417 | 8.838834 | 2001.3 |

Table 4.1.3.1-2 - NAC FM : Calculation of EFL

| UNCERTAINTY <br> (Effect on Effective Focal Length) |  |  |  |
| :---: | :---: | :---: | :---: |
| ANGLES (0.000003 radians) | $\begin{gathered} \text { DISTANCE } \\ (0.00025 \mathrm{~mm}) \end{gathered}$ | RSS | THREE SIGMA |
| 2.1 | -0.1 | 2.1 | 6.2 |
| 2.7 | -0.1 | 2.7 | 8.1 |
| 4.0 | -1.2 | 4.0 | 11.9 |
| 7.3 | -0.3 | 7.3 | 21.8 |
| 7.2 | -0.3 | 7.2 | 21.6 |
| 3.9 | -0.2 | 3.9 | 11.8 |
| 2.7 | -0.1 | 2.7 | 8.1 |
| 2.1 | -0.1 | 2.1 | 6.2 |
| 1.5 | -0.1 | 1.5 | 4.4 |
| 1.9 | -0.1 | 1.9 | 5.8 |
| 2.8 | -0.1 | 2.8 | 8.4 |
| 5.2 | -0.2 | 5.2 | 15.7 |
| 5.2 | -0.2 | 5.2 | 15.7 |
| 2.8 | -0.1 | 2.8 | 8.4 |
| 1.9 | -0.1 | 1.9 | 5.8 |
| 1.5 | -0.1 | 1.5 | 4.4 |
| 2.1 | -0.1 | 2.1 | 6.2 |
| 2.7 | -0.1 | 2.7 | 8.1 |
| 4.0 | -0.2 | 4.0 | 11.9 |
| 7.3 | -0.3 | 7.3 | 21.9 |
| 7.3 | -0.3 | 7.4 | 22.1 |
| 4.0 | -0.2 | 4.0 | 12.0 |
| 2.7 | -0.1 | 2.7 | 8.2 |
| 2.1 | -0.1 | 2.1 | 6.2 |
| 1.5 | -0.1 | 1.5 | 4.4 |
| 1.9 | -0.1 | 1.9 | 5.8 |
| 2.8 | -0.1 | 2.8 | 8.4 |
| 5.2 | -0.2 | 5.2 | 15.7 |
| 5.2 | -0.2 | 5.2 | 15.7 |
| 2.8 | -0.1 | 2.8 | 8.4 |
| 1.9 | -0.1 | 1.9 | 5.8 |
| 1.5 | -0.1 | 1.5 | 4.4 |

Table 4.1.3.1-3 - NAC FM : Estimate of Uncertainty of EFL Measurement


Figure 4.1.3.1-3 - NAC FM Effective Focal Length Measurements

