### 4.1.3.2 WAC FM FOCAL LENGTH AND DISTORTION MEASUREMENT RESULTS

As reported in Reference 4.1.3.2-1

## Reference 4.1.3.2-1 - IOM DQA \# 95-1047, 'WAC F/M Focal Length And Distortion Measurement Results", Edward Motts, October 26, 1995

### 4.1.3.2.1 Scope

This report describes a measurement of the Cassini Wide Angle Camera Flight Model (WAC F/M). The objective of the measurement was to determine focal length and field distortion of the camera optics. The accuracy requirement for the focal length is defined in Cassini document 699-CAS-5-2036-CAL, Imaging Science Subsystem (ISS) Instrument Calibration Requirements Document, Component Level Calibrations as $\pm 0.5 \mathrm{~mm}$. No requirement is established for field distortion at the component level. Measurements were performed in accordance with ISS ELM-506-001-6.10.3.0, Preliminary Version dated August 14, 1995.

### 4.1.3.2.2 Description of Test Method

Measurements of the angles between the NAC/WAC tooling plate optical cube and the WAC grid target were performed using electronic optical theodolites. The theodolites measured angles in a horizontal plane in reference to a porroprism. Angles in a vertical plane were measured with respect to local gravity. Theodolite angles were recorded using a portable computer running the Leica ManCAT software. Refer to Figure 4.1.3.2-1 for the instrument layout.

Determinations of the tooling plate optical cube $-X$ and $+Z$ face normals were performed by autocollimation to those faces. Determination of the grid target locations was performed by superimposing the theodolite telescope reticle over the intersection. Refer to Figure 4.1.3.2-2 for grid intersection locations.

Database file "WACFL1.dbf" containing all measured angles was exported to Excel spreadsheet "ISSDIST.xls" sheet 2 for data reduction.

### 4.1.3.2.3 Data Reduction

Database files were imported into the Excel spreadsheet "ISSDIST.xls" as described above. Refer to Table 4.1.3.2-1 for raw data.

Angle $\varphi$ (the angle in the plane containing a given grid intersection and the center grid intersection) was calculated as the RSS of the two component angles:

$$
\varphi=\sqrt{\left(\Delta H z^{2}+\Delta V^{2}\right)}
$$

Table 4.1.3.2-2 contains calculated values of angle $\varphi$ for each grid intersection. Radial distances " $h$ '" to each grid intersection were calculated from drawing dimensions and are also contained in Table 4.1.3.2-2.

The effective focal length (EFL) was calculated using h' and $\varphi$ for each grid intersection:

$$
E F L=\frac{h^{\prime}}{\tan \varphi}
$$

Finally, the percentage distortion to a grid target intersection is calculated as the percent deviation from the minimum focal length:

$$
\% \text { Distortion }=\frac{E F L_{n}-E F L_{\min }}{E F L_{\min }} * 100 \%
$$

The twist, or rotation about $Z$, of the grid target is determined as follows. The twist of the grid target with respect to local gravity is calculated by the following equation:

$$
\text { Twist }=\arctan \frac{H z_{2}-H z_{1}}{V_{2}-V_{1}}
$$

Where: $\quad H z_{n}=$ the horizontal angle to point $n$ of the target $\mathrm{V}_{\mathrm{n}}=$ the vertical angle to point n of the target.

The rotation with respect to gravity of the optical cube -X face normal is then subtracted from the twist, as shown in Table 4.1.3.2-3. The difference is the rotation of the grid target with respect to the cube -X face normal. This information will be used to map the field distortion to the CCD after optomechanical characterization of the WAC F/M.

### 4.1.3.2.4 Uncertainty Estimate

The calculated measurement uncertainty in the measured focal length is $\pm 0.251 \mathrm{~mm}$ (three $\sigma$ ). Estimation of the uncertainty (error) in the reported angles was accomplished in spreadsheet "ISSDIST.xls" sheet 2.

Random error was estimated by calculating the standard deviation of the theodolite observations. The equation for EFL was then perturbed by the calculated standard deviation to determine the effect on EFL. Then, the EFL equation was perturbed by the stated uncertainty of the grid target, $\pm 25 \mu \mathrm{~m}$. The two random error contributions were then combined by the Root Sum Square (RSS) method. Finally, the RSS was multiplied times three to give a $\pm$ three $\sigma$ uncertainty estimate. Refer to Table 4.1.3.2-4 for calculation of the measurement uncertainty.

Please note that for simplicity the estimation of uncertainty was performed for one grid intersection only, at point "A1." The actual error would probably be greater for a point closer to the center of the target, and less for a point further away. The estimate is still a useful approximation of the measurement accuracy, however.

### 4.1.3.2.5 Test Results

The calculated focal lengths are shown in Table 4.1.3.2-2, along with the percent distortion.
Figure 4.1.3.2-3 graphically represents the measured values. The best fit curve of Figure 4.1.3.2-3 crosses the vertical axis at approximately 200.22 mm , a value close to the expected paraxial focal length of 200 mm .

The maximum focal length measured was at the ends of the grid targets diagonals, at the maximum radial distance. The largest value was 201.1 mm , which differs from the minimum by $0.45 \%$.

The estimated measurement uncertainty of $\pm 0.251 \mathrm{~mm}$ (three $\sigma$ ) meets the Component Level Calibrations requirement of $\pm 0.5 \mathrm{~mm}$ accuracy.


Figure 4.1.3.2-1 - Instrument Layout

$\rightarrow-1=0.50 \mathrm{~mm}$
GRID TARGET
WITH INTERSECTION POINTS


IDENTIFICATION OF GRID INTERSECTION POINTS

Figure 4.1.3.2-2 - Grid Target and Intersection Point Identification

| A1 | 197.59811 | 90.07299 |
| :--- | :--- | :--- |
| A2 | 198.02491 | 90.07284 |
| A3 | 198.45308 | 90.07268 |
| A4 | 198.88201 | 90.07278 |
| A5 | 199.38233 | 90.00086 |
| A6 | 199.88328 | 89.92913 |
| A7 | 200.31204 | 89.92889 |
| A8 | 200.74022 | 89.92870 |
| A9 | 201.16683 | 89.92847 |
| B1 | 197.60112 | 88.22235 |
| B2 | 198.02600 | 88.64600 |
| B3 | 198.45315 | 89.07289 |
| B4 | 198.88155 | 89.50078 |
| B5 | 199.38241 | 90.00109 |
| B6 | 199.88369 | 90.50121 |
| B7 | 200.31233 | 90.92935 |
| B8 | 200.73980 | 91.35561 |
| B9 | 201.16438 | 91.77912 |
| C1 | 199.31016 | 88.21701 |
| C2 | 199.31039 | 88.64382 |
| C3 | 199.31057 | 89.07177 |
| C4 | 199.31063 | 89.50054 |
| C5 | 199.38236 | 90.00105 |
| C6 | 199.45414 | 90.50167 |
| C7 | 199.45455 | 90.93030 |
| C8 | 199.45487 | 91.35810 |
| C9 | 199.45505 | 91.78523 |
| D1 | 201.16209 | 88.22046 |
| D2 | 200.73825 | 88.64442 |
| D3 | 200.31099 | 89.07180 |
| D4 | 199.88305 | 89.50015 |
| D5 | 199.38244 | 90.00100 |
| D6 | 198.88217 | 90.50195 |
| D7 | 198.45416 | 90.93013 |
| D8 | 198.02736 | 91.35687 |
| D9 | 197.60280 | 91.78132 |
| PORROB1 | 109.16174 | 101.18848 |
| PORROC1 | 0.99998 | 91.42705 |
| CUBEX1 | 257.33065 | 89.99270 |
| CUBEZ1 | 91.22379 | 89.99795 |
|  |  |  |
|  |  |  |

Table 4.1.3.2-1 - Raw Data : WAC Flight Focal length and Field Distortion Measurements

| Grid Point | $\mathbf{h}^{\prime}(\mathbf{m m})$ | phi (radians) | EFL (mm) | \% Distortion |
| :---: | :---: | :---: | :---: | :---: |
| A1 | -6.25 | 0.03117 | 200.6 | 0.25 |
| A2 | -4.76 | 0.02372 | 200.5 | 0.15 |
| A3 | -3.26 | 0.01627 | 200.4 | 0.11 |
| A4 | -1.77 | 0.00882 | 200.4 | 0.12 |
| A6 | 1.77 | 0.00883 | 200.1 | 0.00 |
| A7 | 3.26 | 0.01627 | 200.3 | 0.06 |
| A8 | 4.76 | 0.02373 | 200.4 | 0.12 |
| A9 | 6.25 | 0.03117 | 200.6 | 0.23 |
| B1 | -8.84 | 0.04394 | 201.0 | 0.45 |
| B2 | -6.72 | 0.03346 | 200.7 | 0.26 |
| B3 | -4.60 | 0.02292 | 200.5 | 0.16 |
| B4 | -2.47 | 0.01236 | 200.3 | 0.07 |
| B6 | 2.47 | 0.01236 | 200.2 | 0.05 |
| B7 | 4.60 | 0.02293 | 200.4 | 0.12 |
| B8 | 6.72 | 0.03347 | 200.6 | 0.25 |
| B9 | 8.84 | 0.04394 | 201.0 | 0.45 |
| C1 | -6.25 | 0.03116 | 200.7 | 0.26 |
| C2 | -4.76 | 0.02372 | 200.5 | 0.17 |
| C3 | -3.26 | 0.01627 | 200.4 | 0.11 |
| C4 | -1.77 | 0.00882 | 200.3 | 0.09 |
| C6 | 1.77 | 0.00883 | 200.3 | 0.06 |
| C7 | 3.26 | 0.01627 | 200.4 | 0.11 |
| C8 | 4.76 | 0.02372 | 200.5 | 0.18 |
| C9 | 6.25 | 0.03117 | 200.6 | 0.25 |
| D1 | -8.84 | 0.04394 | 201.0 | 0.45 |
| D2 | -6.72 | 0.03347 | 200.6 | 0.23 |
| D3 | -4.60 | 0.02293 | 200.4 | 0.15 |
| D4 | -2.47 | 0.01236 | 200.2 | 0.05 |
| D6 | 2.47 | 0.01236 | 200.3 | 0.07 |
| D7 | 4.60 | 0.02292 | 200.5 | 0.16 |
| D8 | 6.72 | 0.03346 | 200.7 | 0.28 |
| D9 | 8.84 | 0.04393 | 201.1 | 0.45 |

Table 4.1.3.2-2 - WAC Flight : Calculation of Focal Length and Field Distortion

| ROTATION ABOUT Z |  |
| :---: | :---: |
| Gridline B | $\arctan (\mathrm{Hz2} 2 \mathrm{~Hz} 1) / \mathrm{V} 2-\mathrm{V} 1)=$ |
| Gridline C | 45.0521614 |
| Minus rotation of Cube | -44.987302 |
| Gridline B | 89.99270 |
| Gridline C | -44.94054 |

Table 4.1.3.2-3 - WAC Flight : Calculation of Twist about Optical Axis

| UNCERTAINTY ESTIMATE |  |  |
| :--- | :---: | :---: |
| The effect on EFL of perturbing | BY | EFFECT |
| Horizontal and Vertical Angles | $0.0002^{\circ}$ | 0.023 mm |
| Distance $\mathrm{h}^{\prime}$ | 25 micrometer | 0.1 mm |
| RSS of above | 0.084 |  |
| RSS $\times 3$ | 0.251 |  |

Table 4.1.3.2-4 - WAC Flight: Estimate of Uncertainty in Measured EFL

EFL vs $h^{\prime}$


Figure 4.1.3.2-3 - WAC FM Effective Focal Length Measurements

